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EXAMPLE OF INTERACTION EFFECTS IN TRANSDUCER ARRAYS. PART II.(U)
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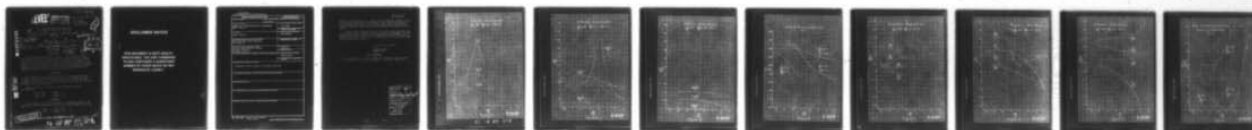
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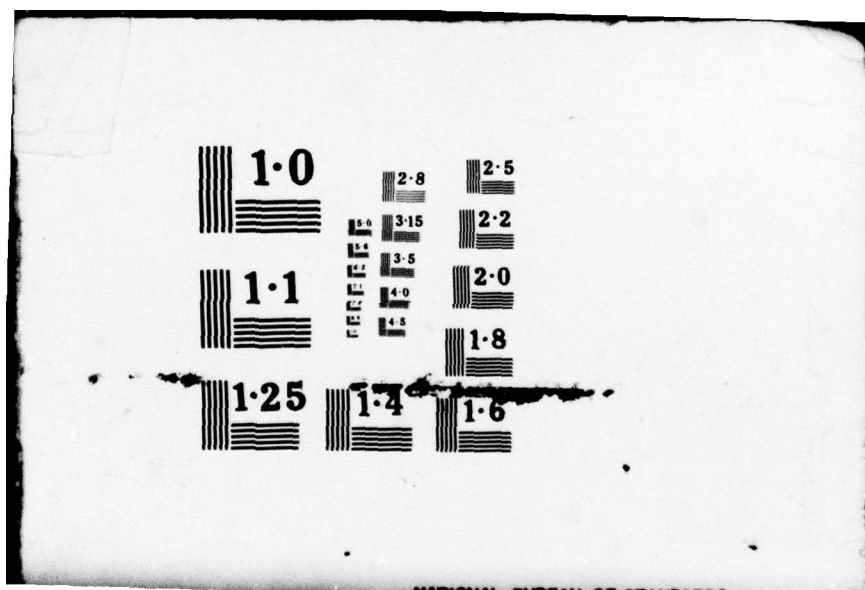
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EXAMPLE OF INTERACTION EFFECTS IN TRANSDUCER ARRAYS, PART II

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by
Judith F. Atwood

USL Technical Memorandum No. 912-44-62-77-2

25 May 1962

INTRODUCTION

The material presented here is an extension of the memorandum "Example of Interaction Effects in Transducer Arrays" by Sherman and Atwood (reference (a)). The array concerned consists of one circular piston surrounded by six other pistons in an infinite rigid baffle. The value of ka specified for each element is $ka = .5$. Calculations for piston velocities and radiation impedance are made for given spacings and individual transducer efficiency, while varying the internal mechanical reactance X_m . The power and the mechanoacoustical efficiency of the array are also shown as functions of X_m .

CALCULATIONS

The variable used in this case is the ratio of the internal mechanical reactance to the self radiation reactance, X_m/X_{11} . The resonant frequency of a single isolated transducer, at which the previous calculations were made, corresponds to an $X_m/X_{11} = -1$. All other conditions and notations are the same as those used by Sherman and Atwood.

Three combinations of spacing and single transducer efficiency are considered:

$d/2a = 1.86$	$RM/R_{11} = .11$
$d/2a = 1.18$	$RM/R_{11} = .11$
$d/2a = 1.18$	$RM/R_{11} = 1.0$

CONCLUSIONS

A small change in X_m might be considered to be caused by a change in the frequency. The relationship between X_m and the frequency change, $\Delta\omega = \omega - \omega_{11}$, is:

$$\frac{\Delta\omega}{\omega_{11}} \approx \frac{\gamma X_{11}}{2 Q_{11} R_{11}} \left(\frac{X_m}{X_{11}} + 1 \right)$$

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$$\left(1 - \frac{X}{R}\right) \frac{X}{R} = \frac{X}{R} - \frac{X^2}{R^2}$$

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REPORT DOCUMENTATION PAGE		READ INSTRUCTIONS BEFORE COMPLETING FORM
1. REPORT NUMBER	2. GOVT ACCESSION NO. 912-44-62	3. RECIPIENT'S CATALOG NUMBER
4. TITLE (and Subtitle) EXAMPLE OF INTERACTION EFFECTS IN TRANSDUCER ARRAYS: PART II		5. TYPE OF REPORT & PERIOD COVERED Tech. Memo.
		6. PERFORMING ORG. REPORT NUMBER S-F001 03 04-8044
7. AUTHOR(s) Atwood, Judith F.		8. CONTRACT OR GRANT NUMBER(s) Nonr-266(84)
9. PERFORMING ORGANIZATION NAME AND ADDRESS Naval Underwater Sound Laboratory New London, CT		10. PROGRAM ELEMENT, PROJECT, TASK AREA & WORK UNIT NUMBERS
11. CONTROLLING OFFICE NAME AND ADDRESS Office of Naval Research, Code 221 800 North Quincy St. Arlington, VA 22217		12. REPORT DATE 25 MAY 62
		13. NUMBER OF PAGES
14. MONITORING AGENCY NAME & ADDRESS (if different from Controlling Office)		15. SECURITY CLASS. (of this report) UNCLASSIFIED
		15a. DECLASSIFICATION/DOWNGRADING SCHEDULE
16. DISTRIBUTION STATEMENT (of this Report) Approved for public release; distribution unlimited.		
17. DISTRIBUTION STATEMENT (of the abstract entered in Block 20, if different from Report)		
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where Q_{11} is the mechanical Q of a single isolated transducer in water, and ω_{11} is the resonant frequency of that transducer. Thus, Figure 9 shows that, for the loose-packed case ($d/2a = 1.86$), a slight variation from the individual transducer resonance increases the array's mechanoacoustic efficiency significantly.

It may be pointed out again that, for the velocity limited situation, the use of highly efficient elements in such an array has disadvantages. The power radiated by the array (Figure 8) is considerably lower, and the efficiency of the whole array (Figure 9) is subject to much sharper variations when the single transducer efficiency is high.

Judith F. Atwood

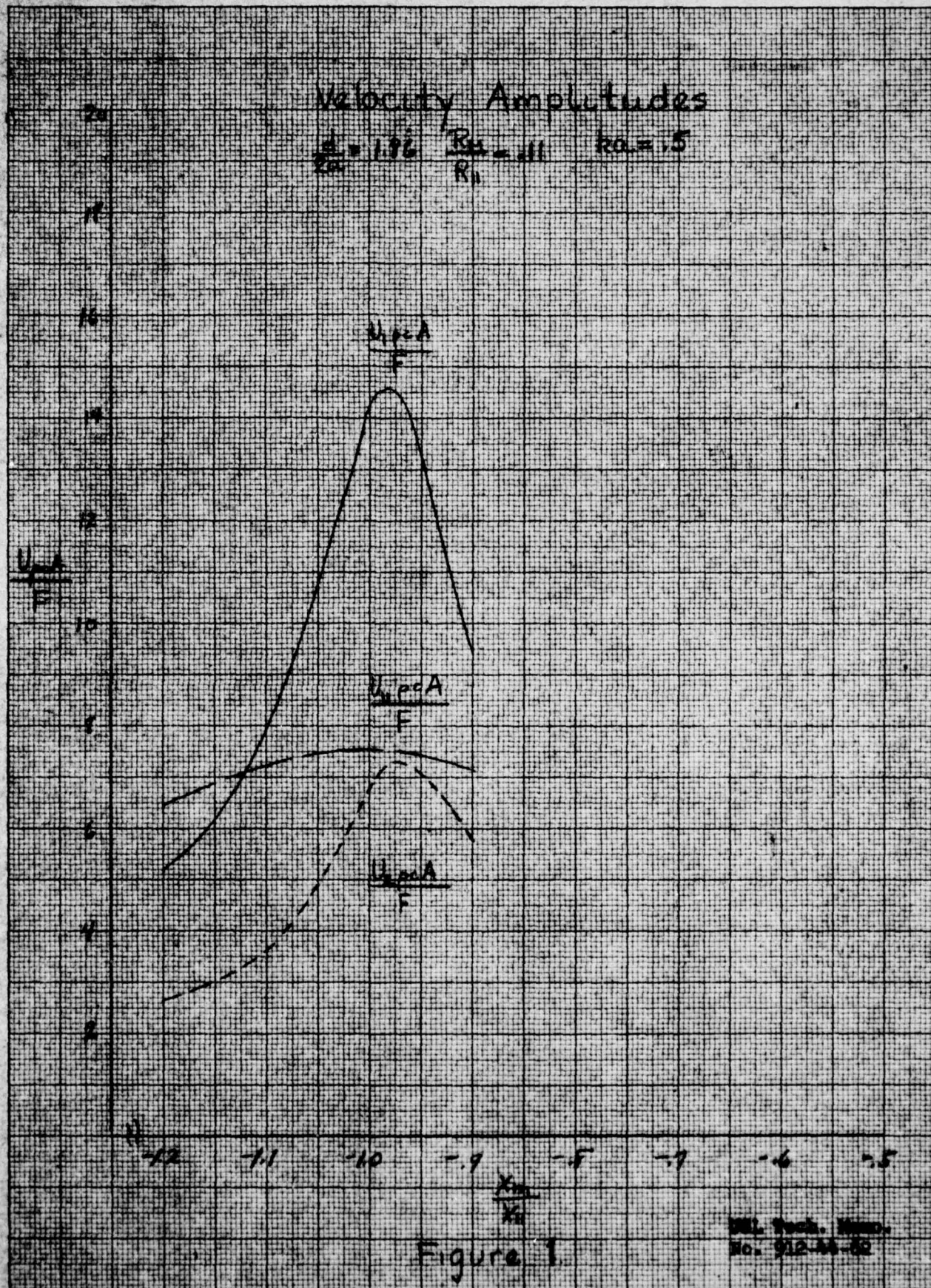
JUDITH F. ATWOOD
Mathematician

LIST OF REFERENCES

- (a) C. H. Sherman and J. F. Atwood, "Example of Interaction Effects in Transducer Arrays", USL Technical Memorandum No. 912-20-62, 1 March 1962

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Velocity Amplitudes

$$\frac{d}{2a} = 1.13 \quad \frac{R_1}{R_2} = .11 \quad R_2 = .5$$

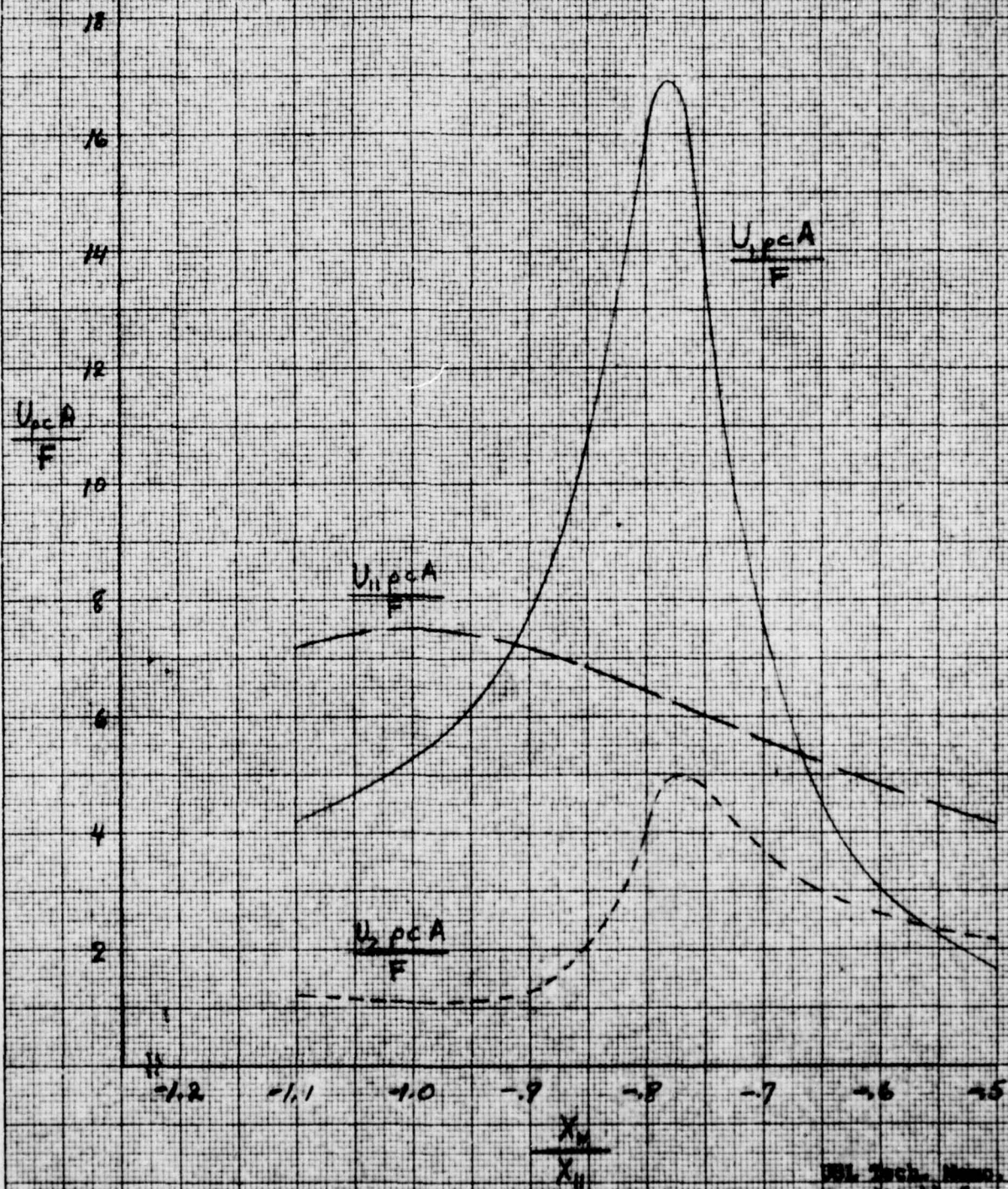
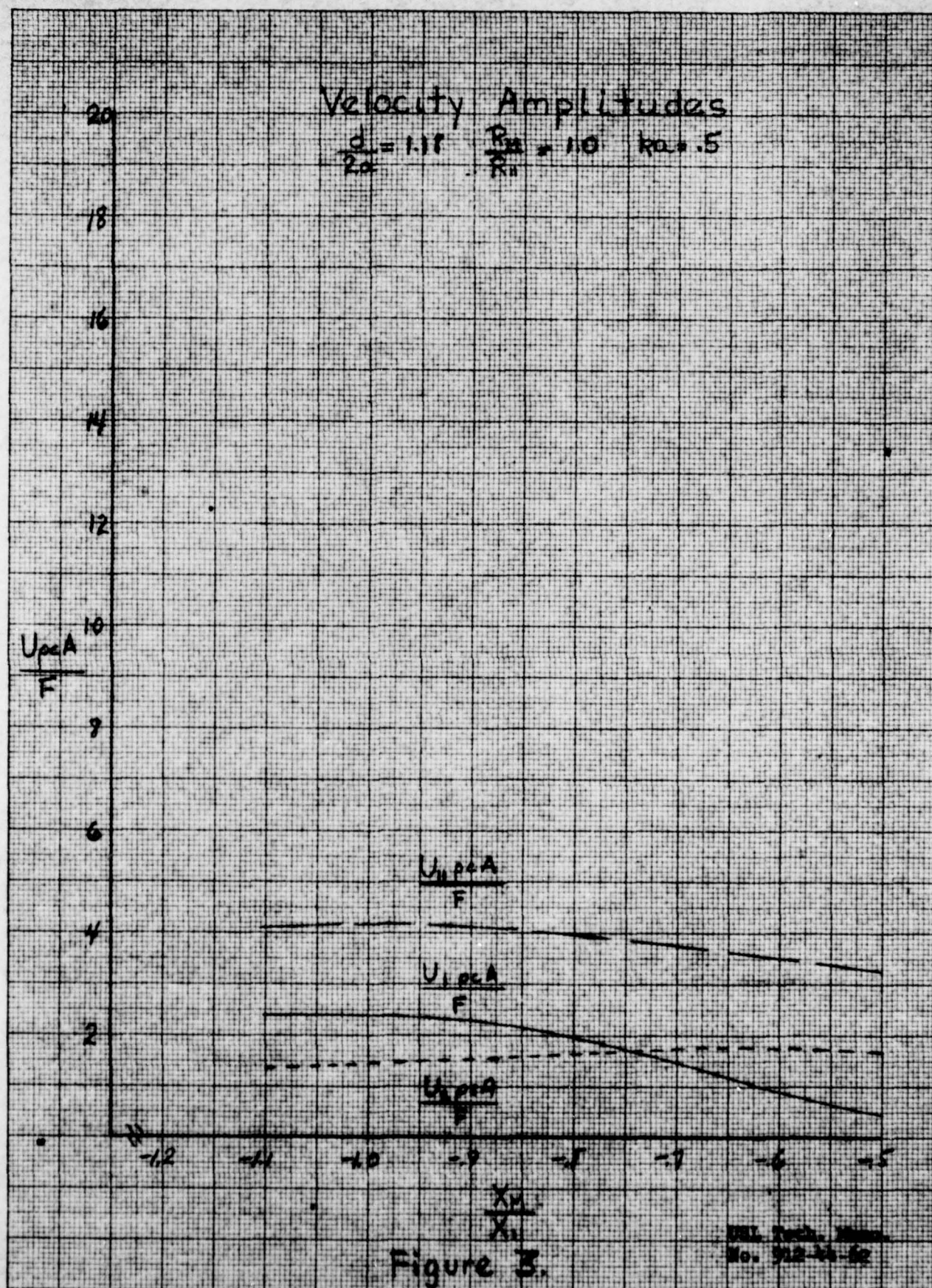
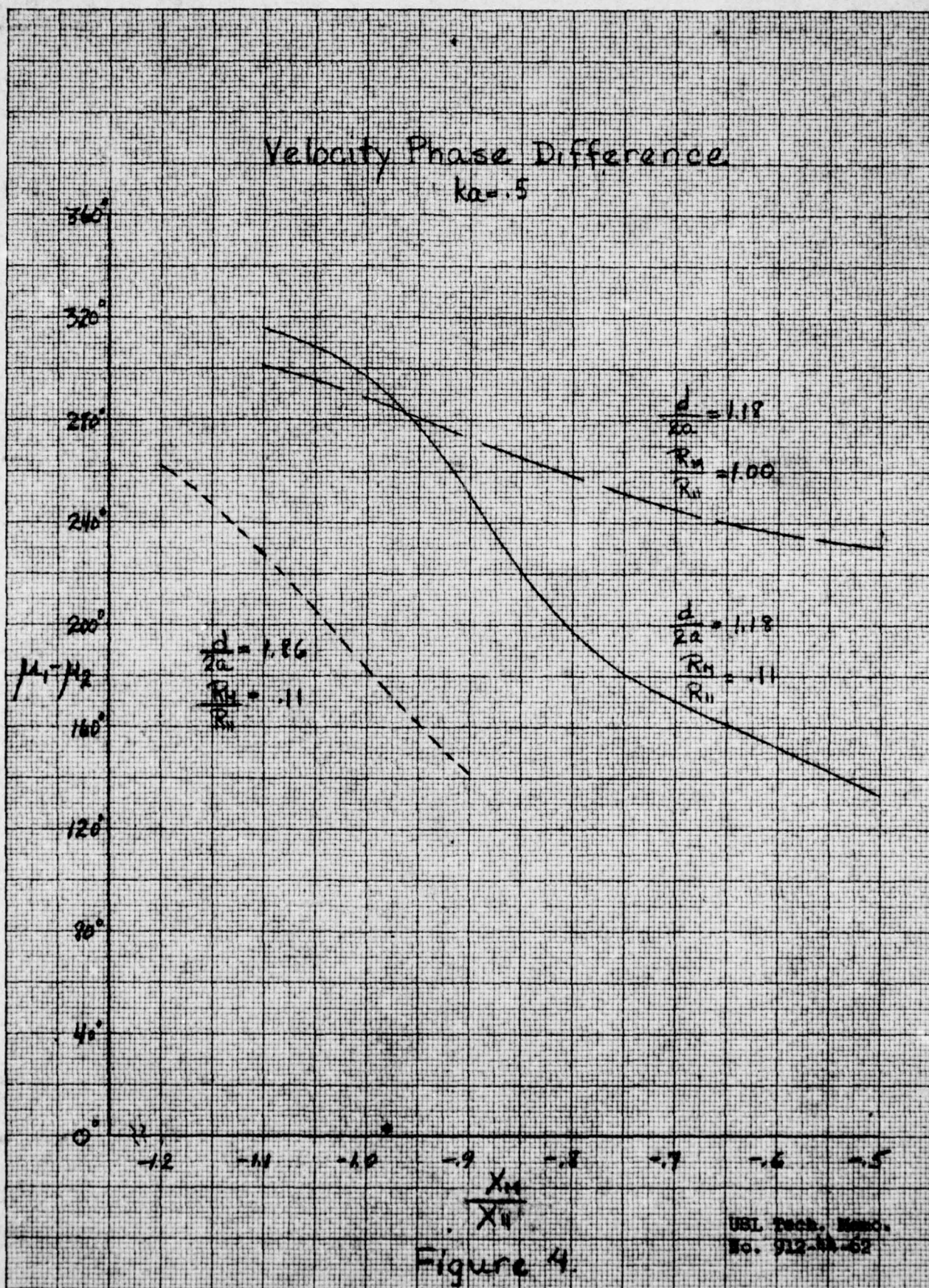


Figure 2.





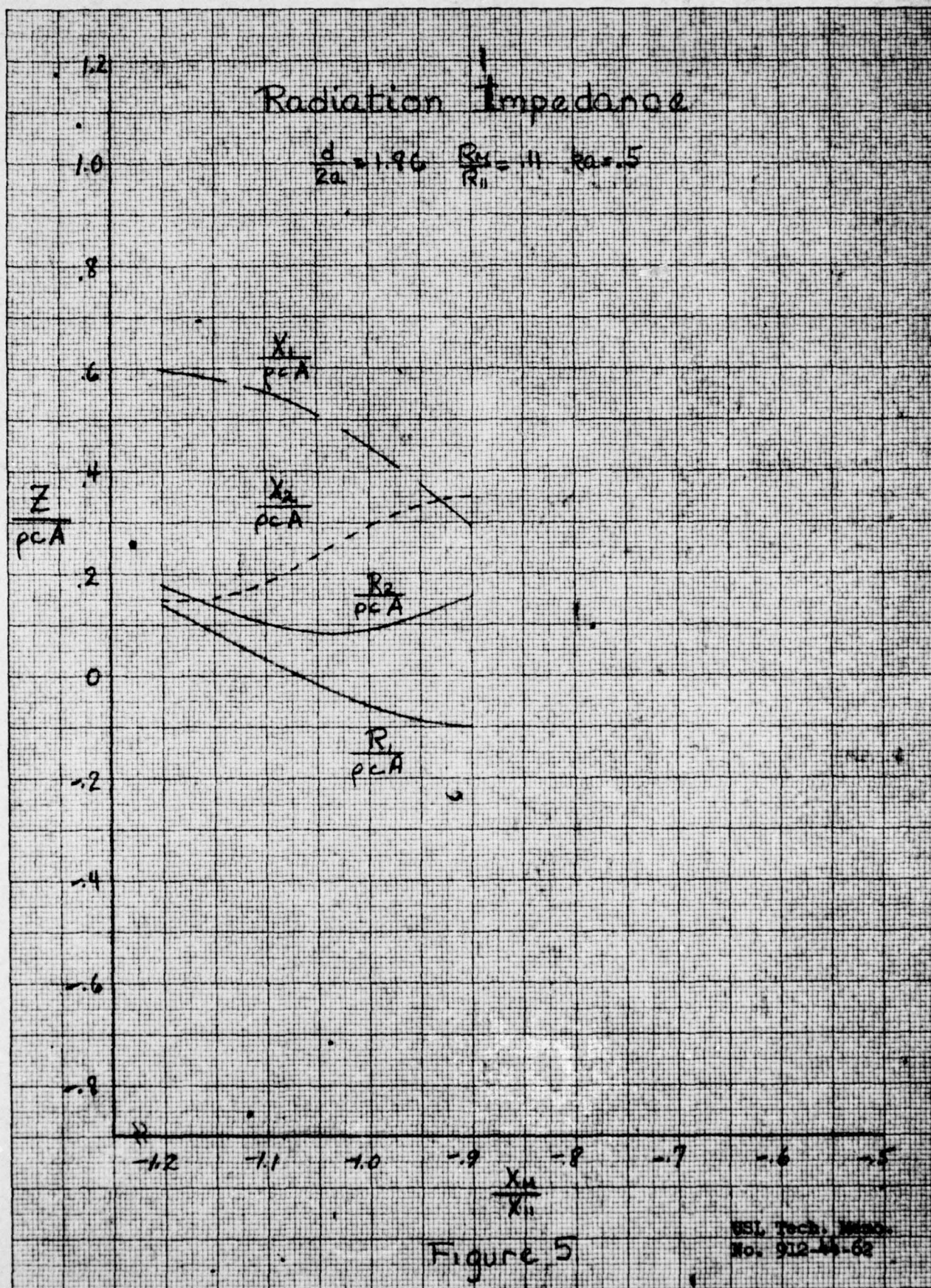
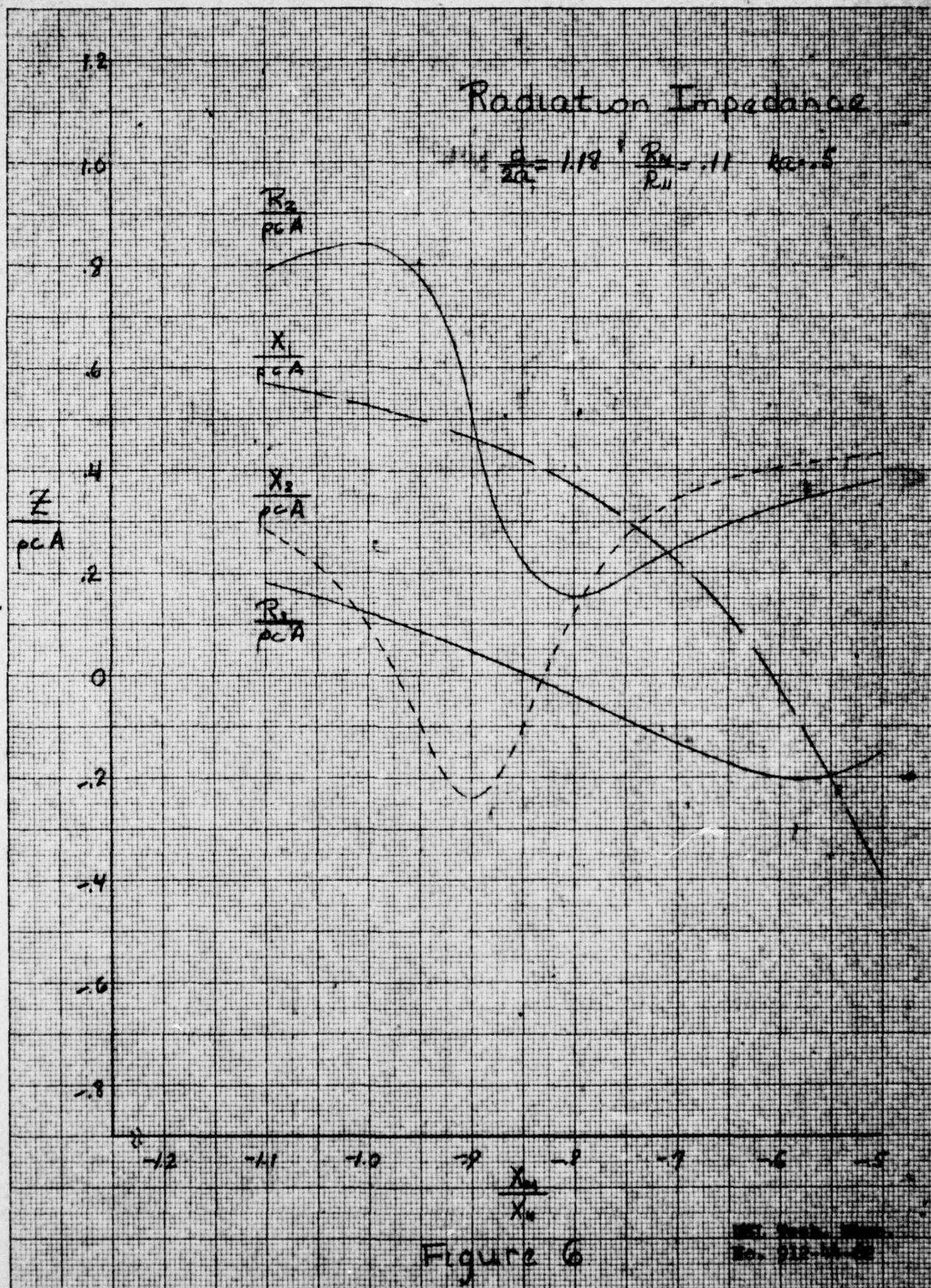
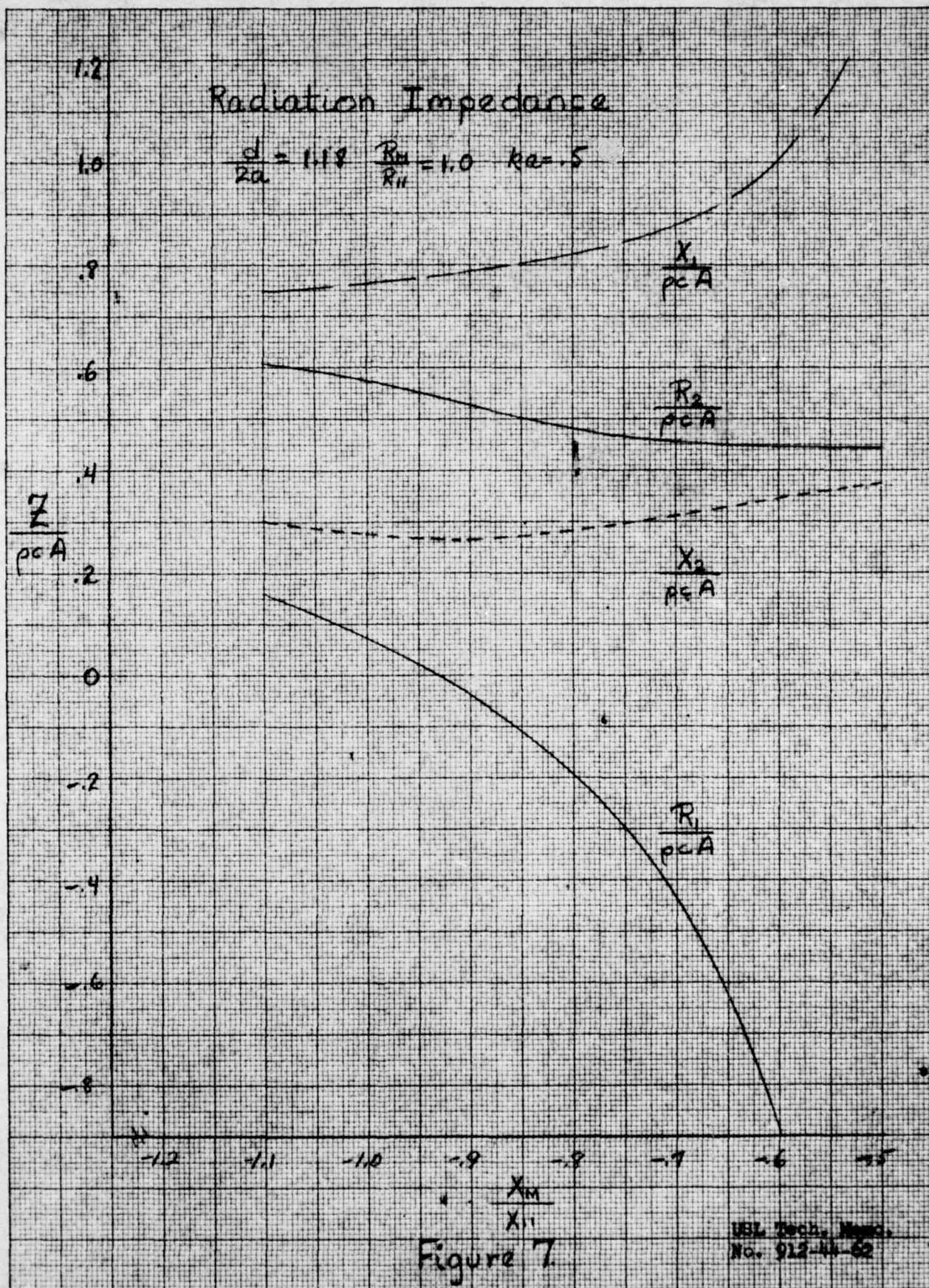
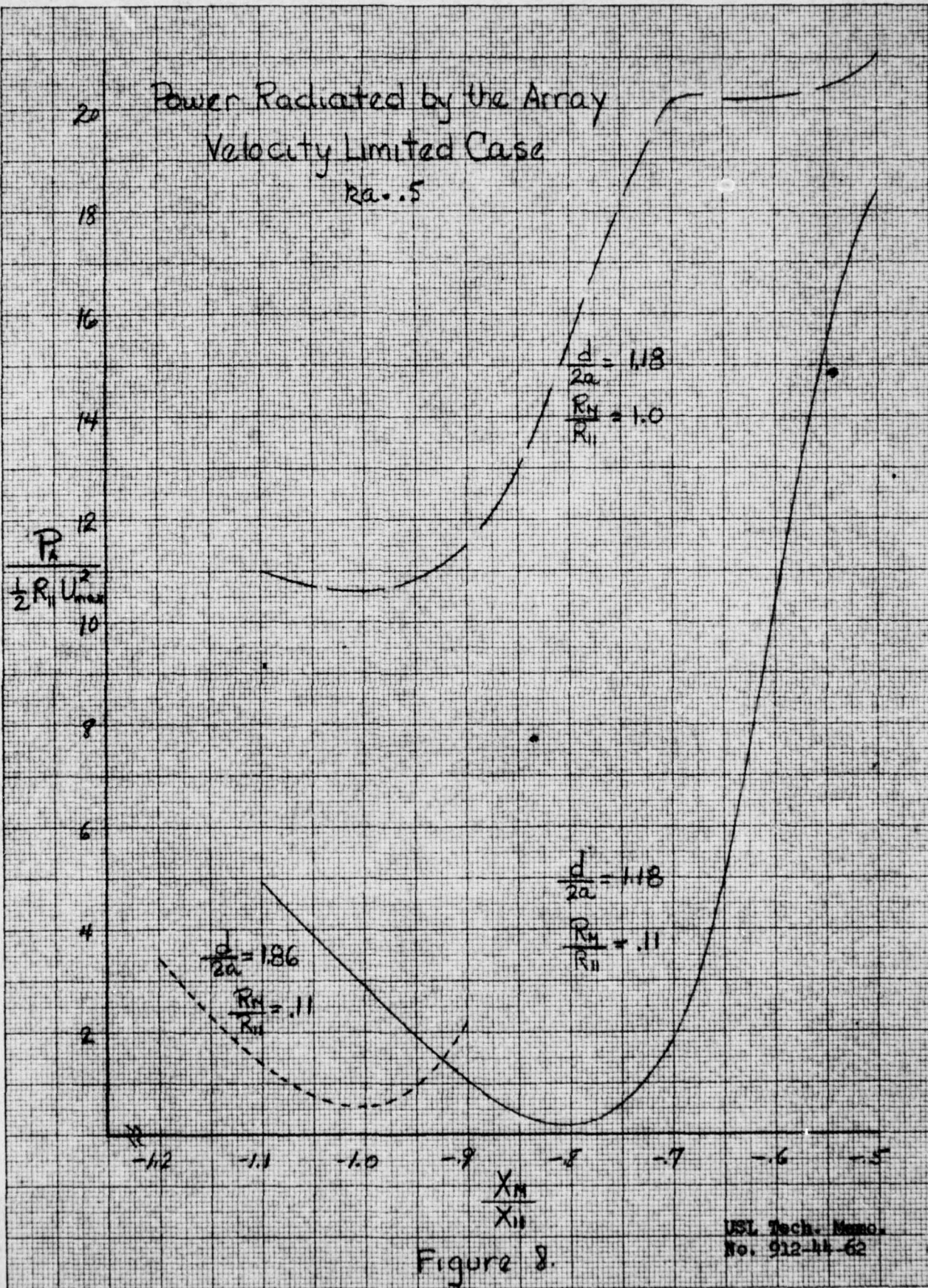


Figure 5







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10 Mechanoacoustical Efficiency of the Array $R_d = .5$

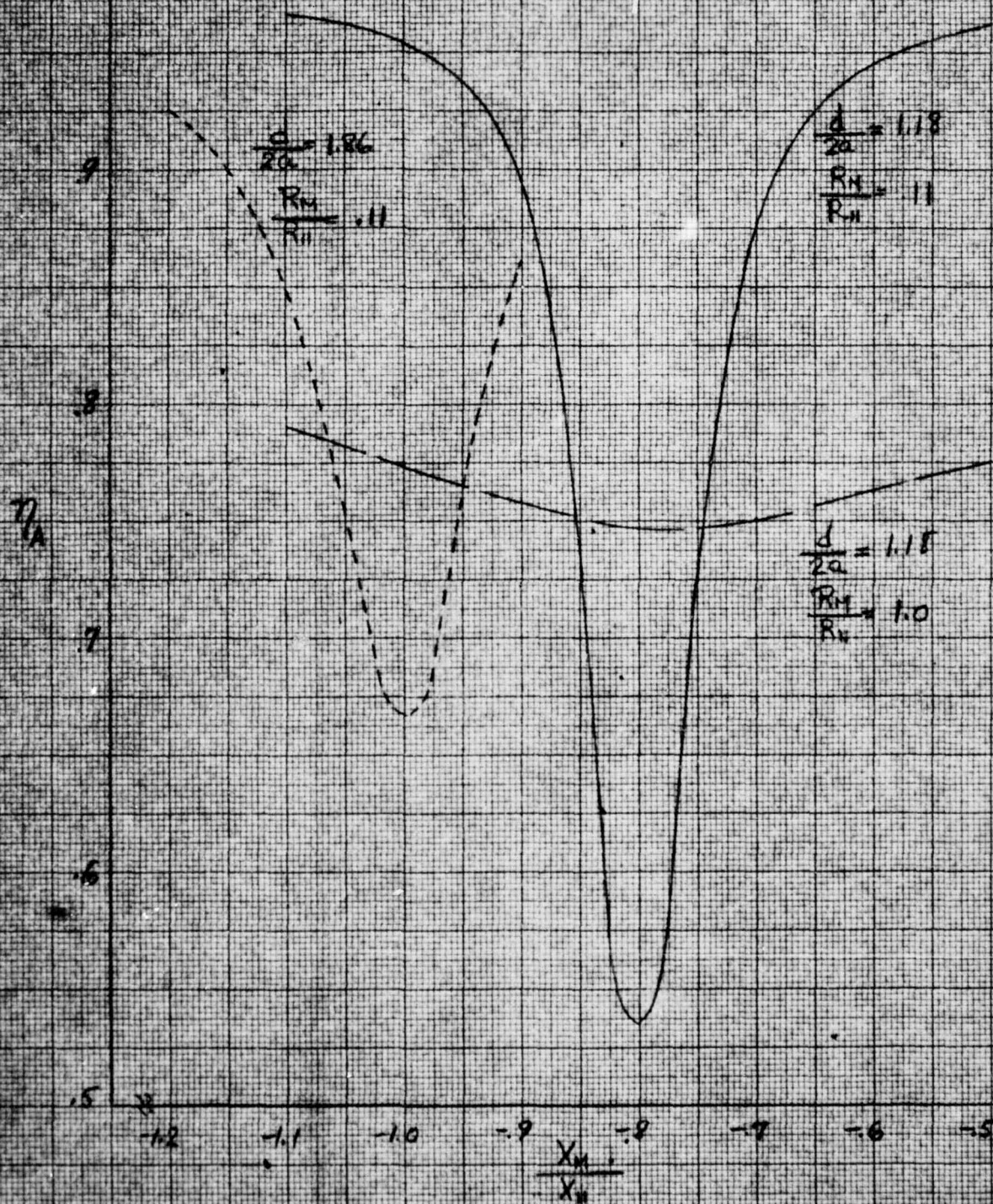


Figure 9.

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